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Failure of two porous sandstones under true triaxial conditions

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ABSTRACT

The role of the intermediate principal stress in rock failure has been a subject of continuing debate since the pioneering work of Mogi in the 1960s with true triaxial tests. These are tests in which all three principal stresses are different, $\sigma_1, \sigma_2, \sigma_3$, positive in compression. In recent years, an increase in data from such tests, some at constant Lode angle and/or constant mean stress, has provided additional fodder for discussion. Here, we analyze the results of tests on true triaxial data from two porous sandstones, Coconino [1] and Bentheim [2]. The tests are of two types: conventional tests which are fixed and are increased to failure; and novel tests which are fixed and are increased so that the ratio has fixed values: 0, 1/6, 1/3, 1/2, and 1, corresponding to Lode angles of 0° and 90° . The analysis is based on a modified form of the Matsuoka–Nakai/Lade–Duncan condition, employed earlier by Haimson and Rudnicki [3] for the prediction of fault angle:

where θ is determined by the mean stress dependence in deviatoric pure shear ($\sigma_1 = \sigma_2 = \sigma_3$). θ controls the shape of the failure surface in deviatoric planes: For $\theta = 0^\circ$ the shape is circular, as for a Drucker-Prager material; for $\theta = 90^\circ$, the shape is triangular, as for a Rankine material. Dependence of θ on σ_1 allows changes of shape of the failure surface with mean stress.

For both sandstones, data for $\theta = 0^\circ$ are well-fit by a quadratic function for σ_1 . Data for the Coconino are consistent with a positive slope for $\theta = 0^\circ$ whereas those for the Bentheim sandstone suggest a peak in the curve. The dependence of θ on σ_1 is determined from the values calculated for $\theta = 0^\circ$. For both sandstones θ is approximated by a bi-linear function of σ_1 . For the Coconino remains positive in the range of the data but for the Bentheim becomes negative for greater than about 180 MPa. This feature appears to be related to the peak in the curve. Curves calculated for θ at other values of σ_1 fit the data well. These forms for θ and σ_1 are used with the above criterion to calculate results for conventional true triaxial tests and compare with observations. The calculated results exhibit the typical behavior that at failure for fixed σ_1 increases to a peak and then decreases with increasing σ_2 . Agreement with the data is generally good, although less so for axisymmetric stress states.

REFERENCES

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